



Sistemas de transmissão em Corrente Contínua

DC Transmission Systems.

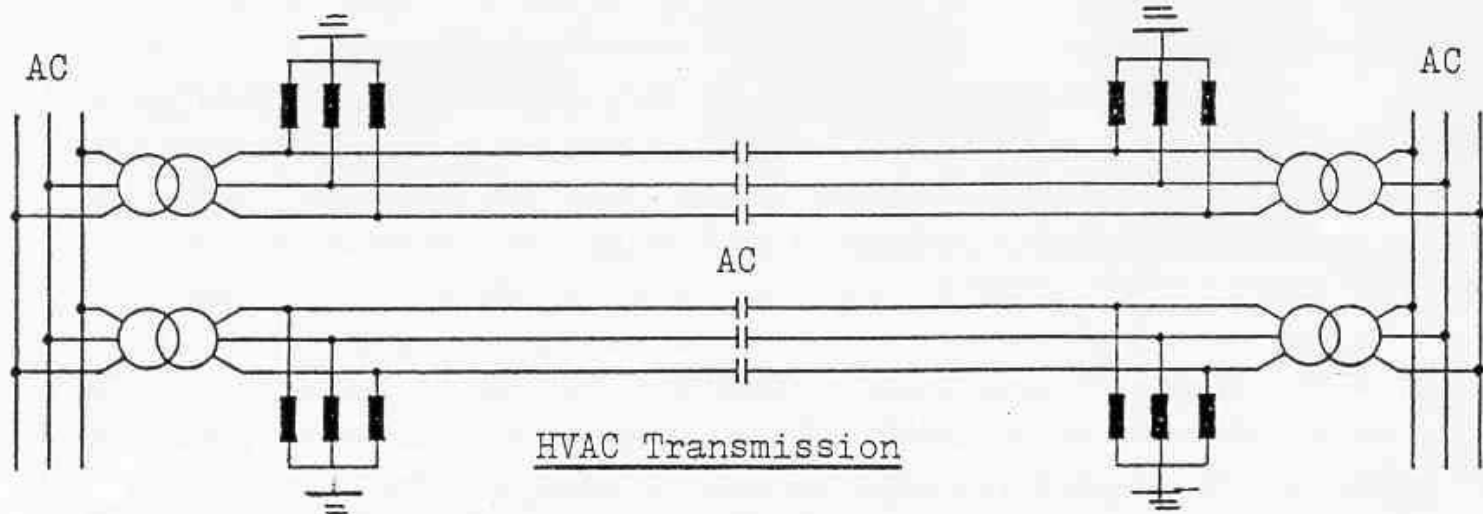
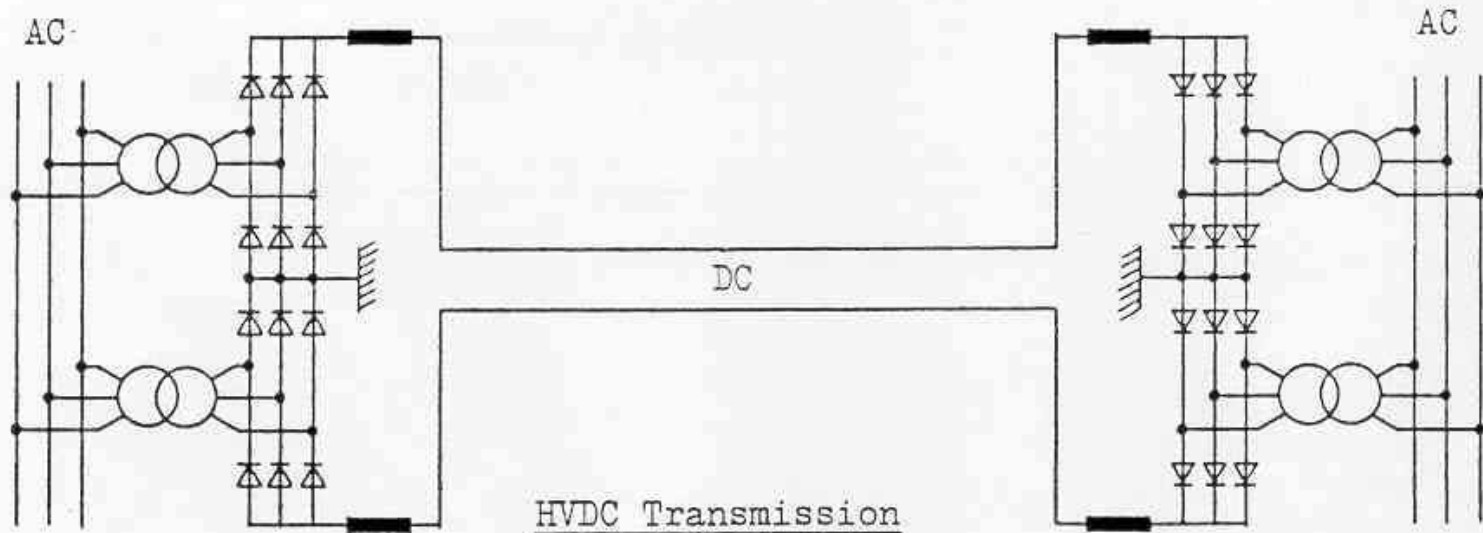
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Sumario

- **Como é constituído o sistema CC**
- **Como é constituído o sistema CA**
- **Comparação CA-CC**
- **Princípio de funcionamento**
- **Sistemas CC em operação e futuros**



Additional costs for converter stations in the HVDC transmission are balanced by savings in the transmission line itself

Corrente Alternada

Custo da linha = $(A + B S) L$

Custo das perdas = $\frac{C}{S} L = L r \left(\frac{P}{V} \right)^2 \frac{1}{S}$

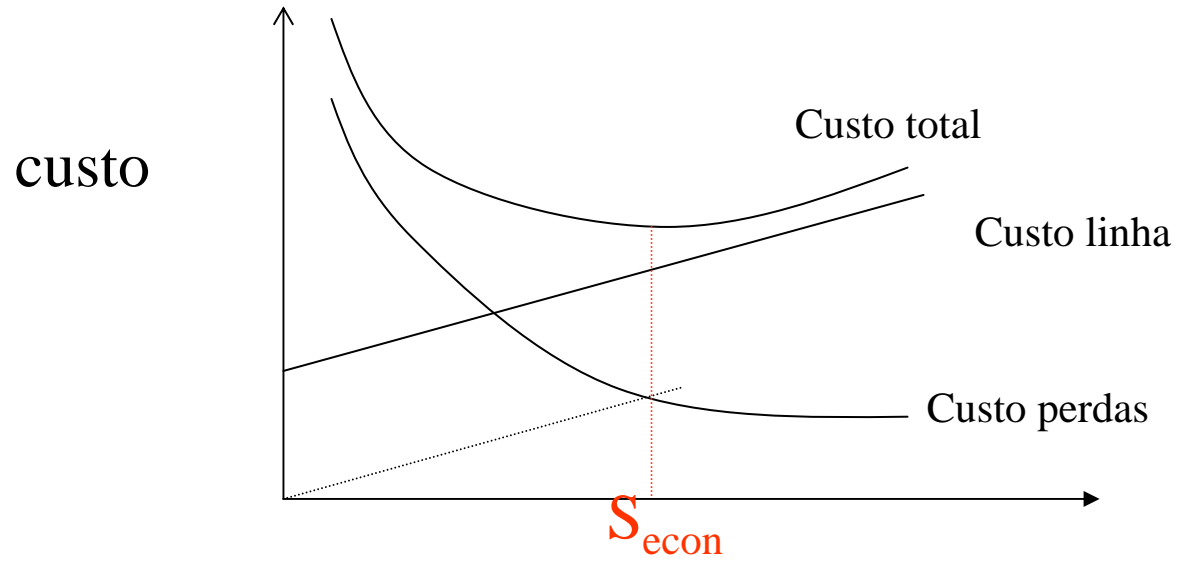
L=comprimento

S= secção Alumínio

Ct = Custo Total = $A + B S + \frac{C}{S}$ $\frac{dCt}{ds} = B - \frac{C}{S^2} = 0 \Rightarrow S_{ec} = \sqrt{\frac{C}{B}} = \sqrt{\frac{D}{B}} \left(\frac{P}{V} \right)$

Condutor econômico depende potência e tensão
independe do comprimento.

Condutor econômico



S

Tensão Econômica CA

| kV | MW |
|-----------|-------------|
| 345/362 | 500 - 700 |
| 500/525 | 1000 - 1500 |
| 760/765 | 2000 - 3000 |
| 1000/1050 | 4000 - 6000 |

Corrente Contínua

$$\text{Custo sistema cc} = C_{conv} + (A + B S + \frac{C}{S}) L = C_{scc}$$

$$C_{conv} = f(V, P)$$

Existe também uma tensão econômica

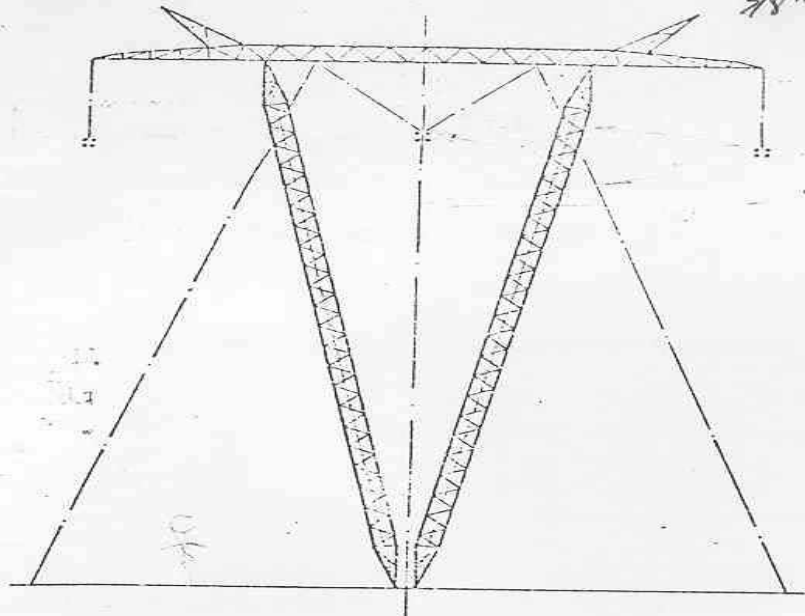
$$V_{econ} = \frac{dC_{scc}}{dV} = 0$$

Problema

- Transmissão de 3.000 MW
- 2.000 km

CA OU CC?

Itaipu =>CA 6300MW 3X765 kV
.....CC 6300MW 2X600kV

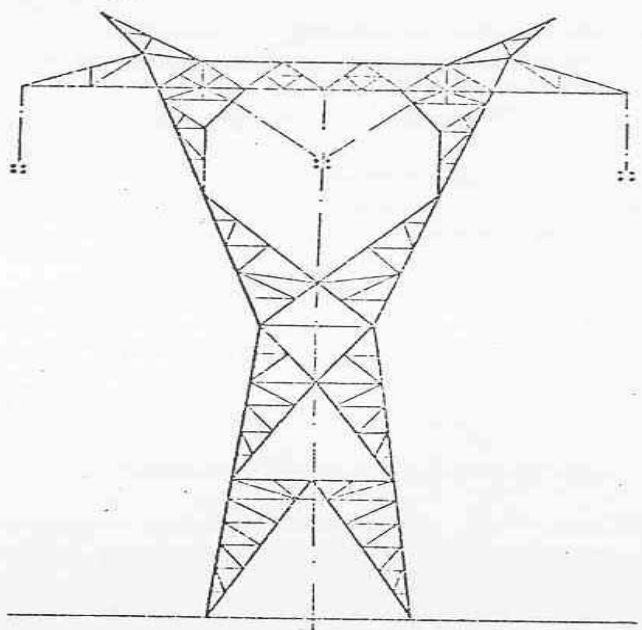


3/8" EHS

TORRE ESTAIADA
 espessura da torre : $w = 1,2$

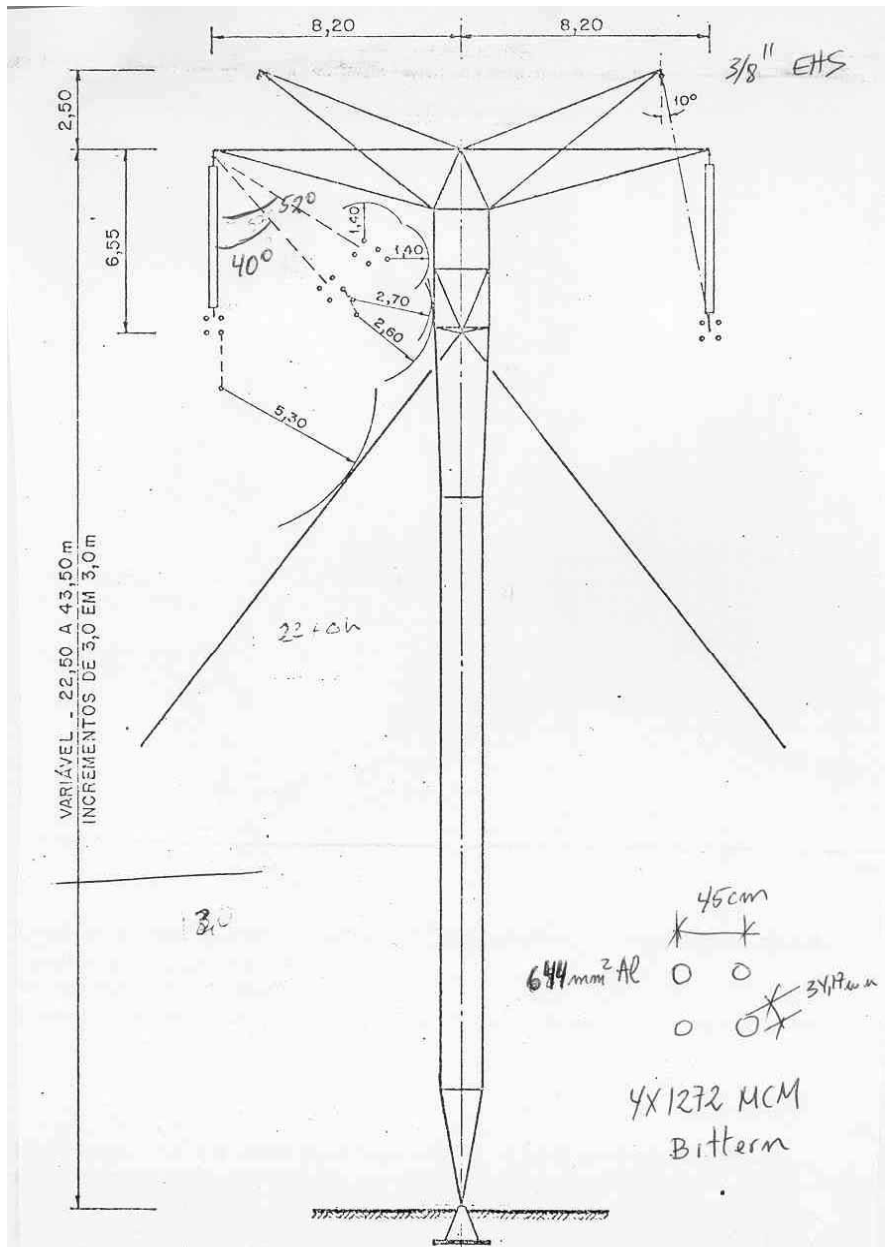
564 mm² AR

* 45 cm
 O O
 O O * 31,98 m m



4X1113 MCM Bluejay

TORRE AUTOPORTANTE
 espessura da torre : $w = 2,4$



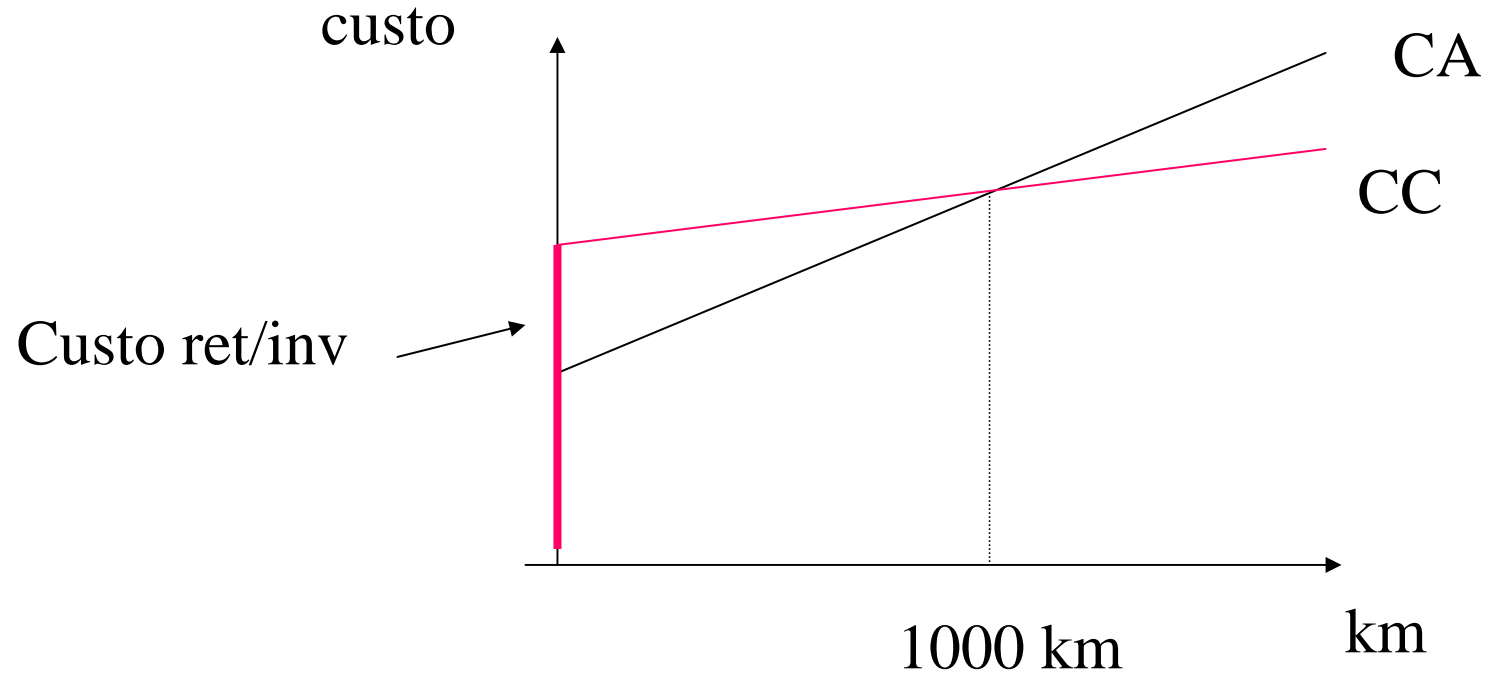
VARIÁVEL - 22,50 A 43,50m
INCREMENTOS DE 3,0 EM 3,0m

3,0

TORRE ESTAIADA TÍPICA

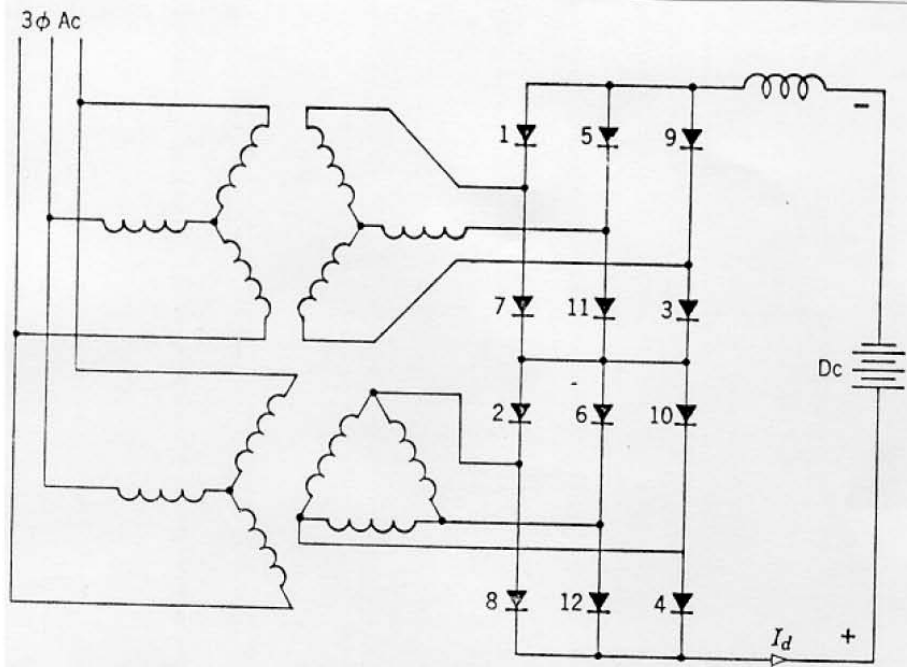
45cm
 644 mm² AR
 3/8" EHS
 4x1272 MCM
 Bitterm

Custos comparativos



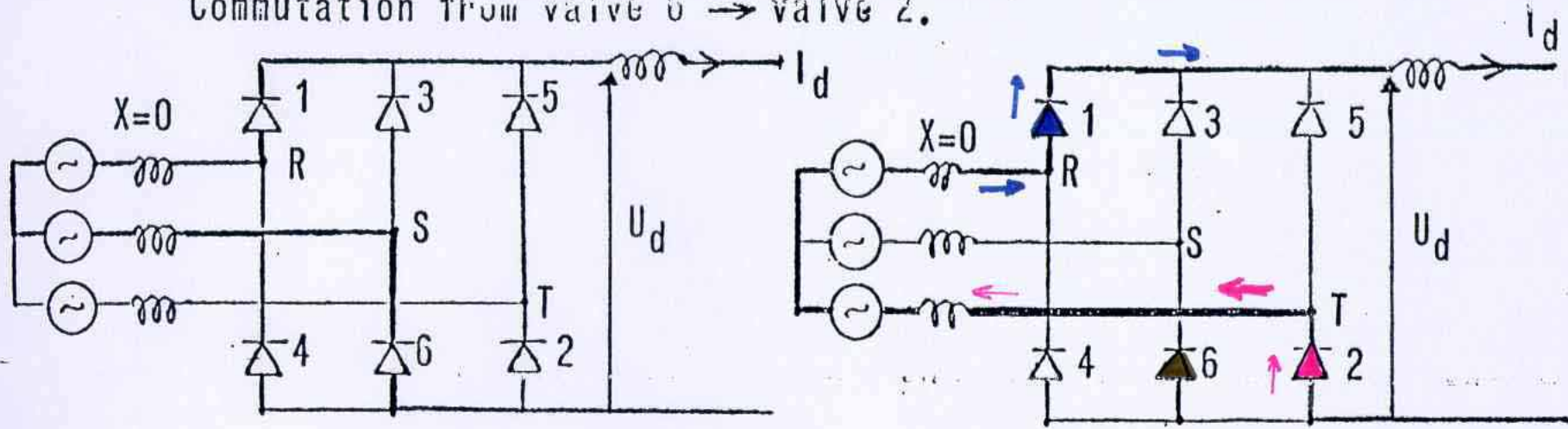
Outras situações onde CC e melhor

- suprimento de energia para ilhas
- sistemas com frequência diferentes
- sistemas com potencial problemas de estabilidade eletromecânica

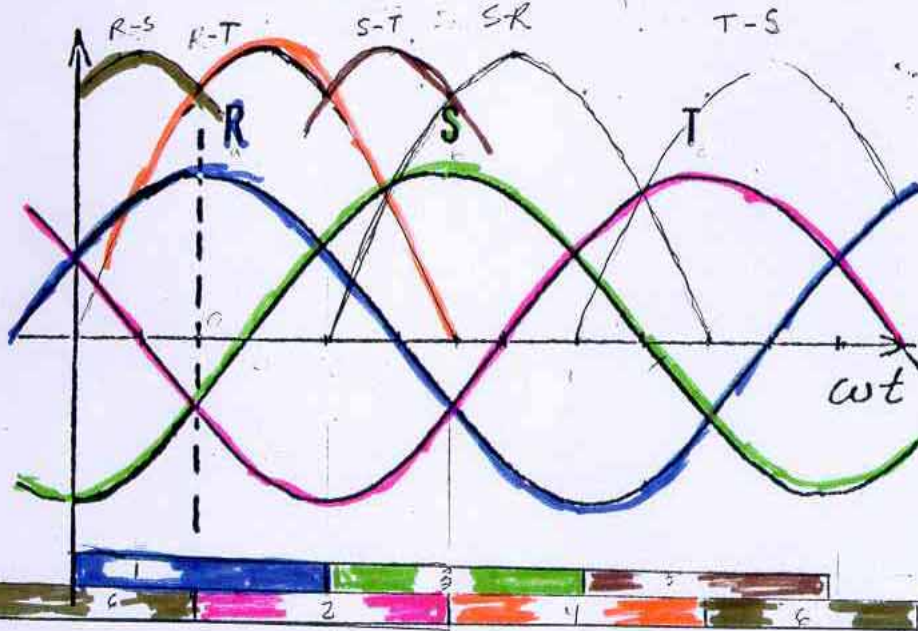


Twelve-pulse cascade of two three-phase bridges.

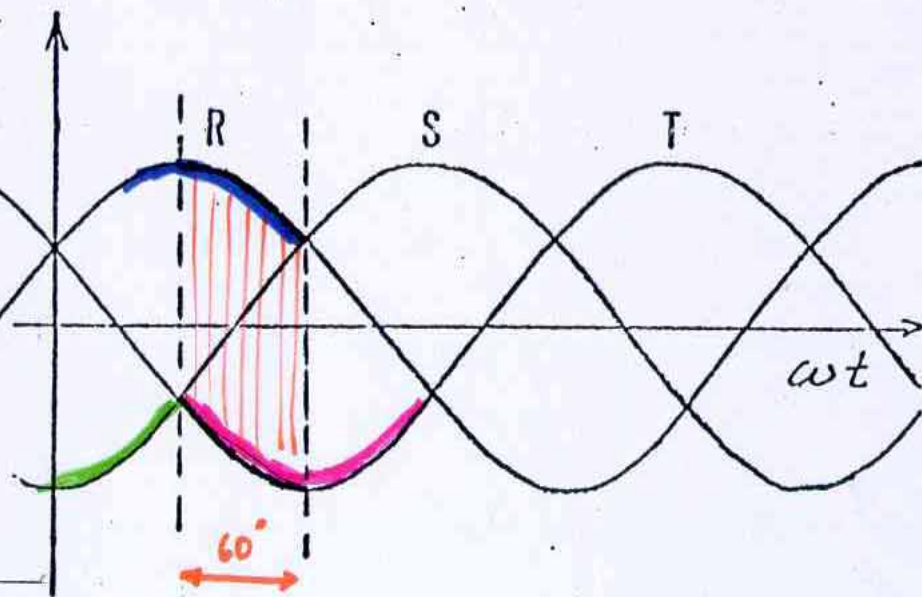
Figure 3 The two-way 6-pulse convertor with uncontrolled valves.
 Commutation from valve 6 \rightarrow valve 2.



Phase voltages

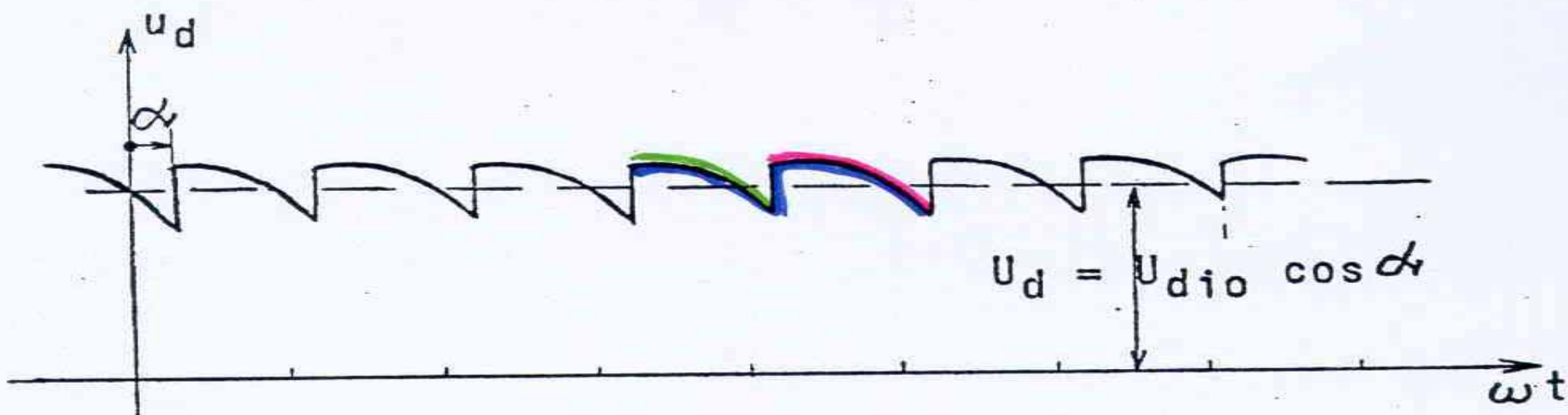
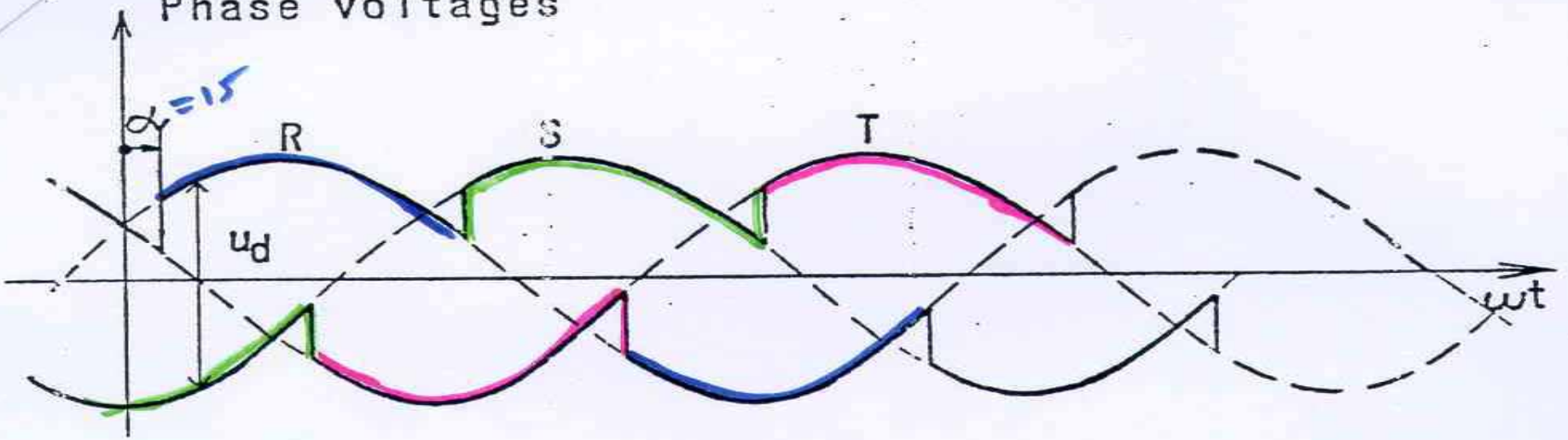


Phase voltages



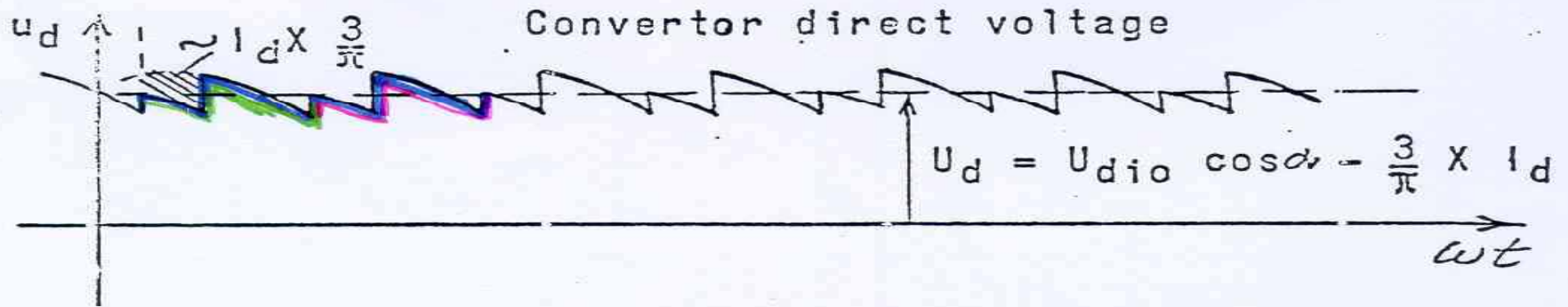
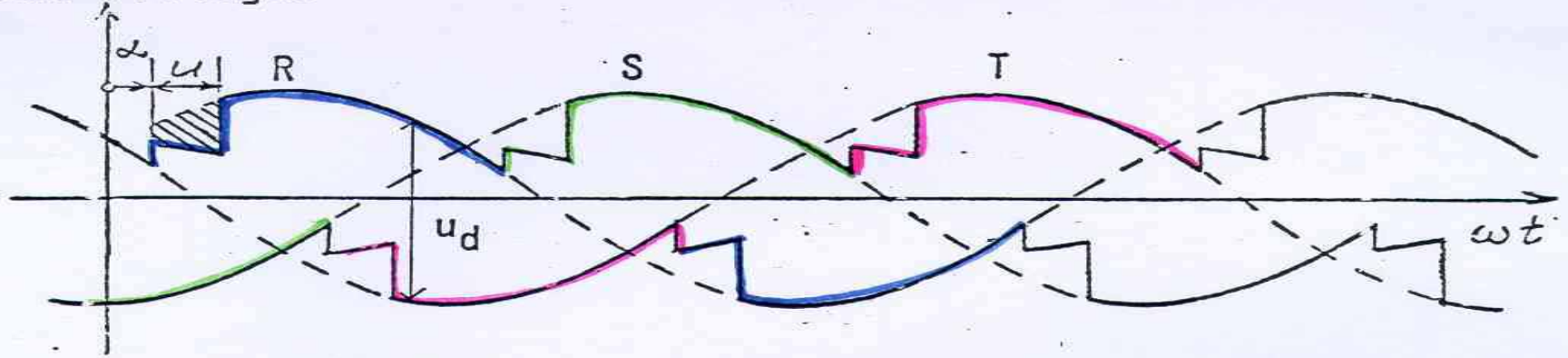
The two-way 6-pulse converter with controlled valves. $X = 0$, $\alpha = 15^\circ$

Phase voltages

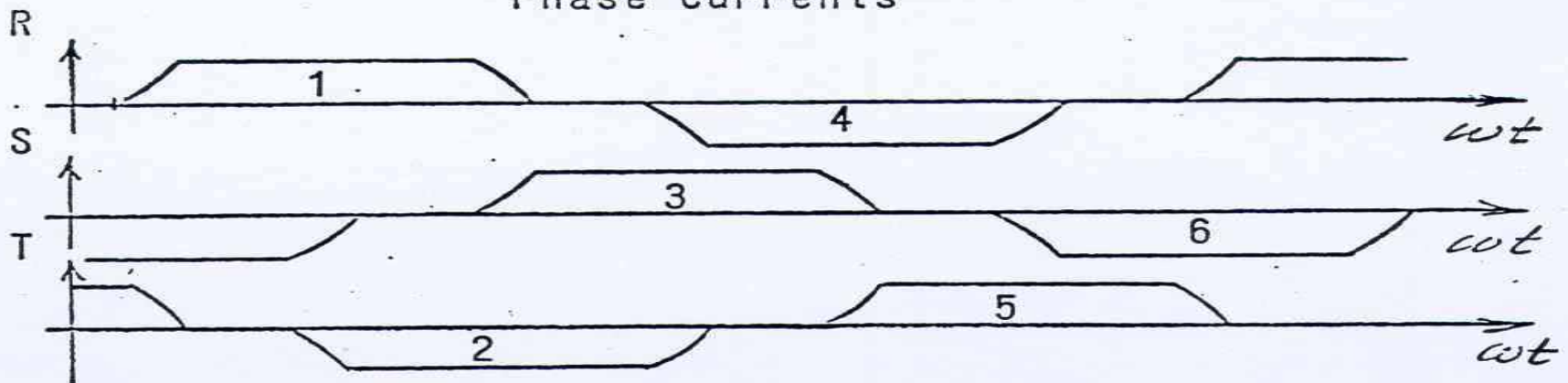


The two-way 6-pulse convertor with controlled valves, $X \neq 0$

Phase voltages



Phase currents



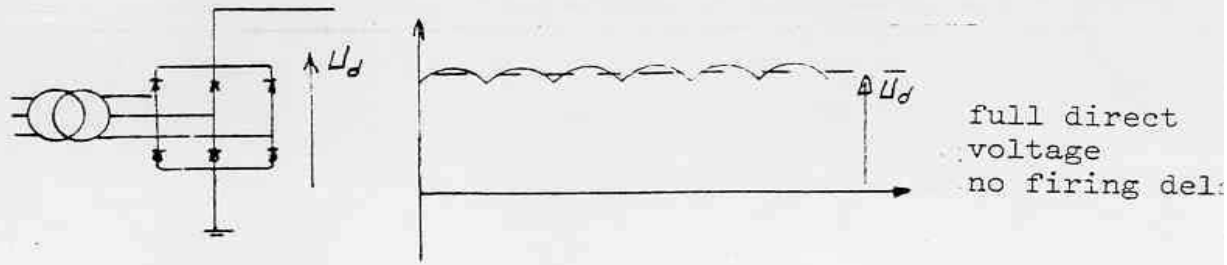


Fig. 1a

Convertor acts as an active power generator

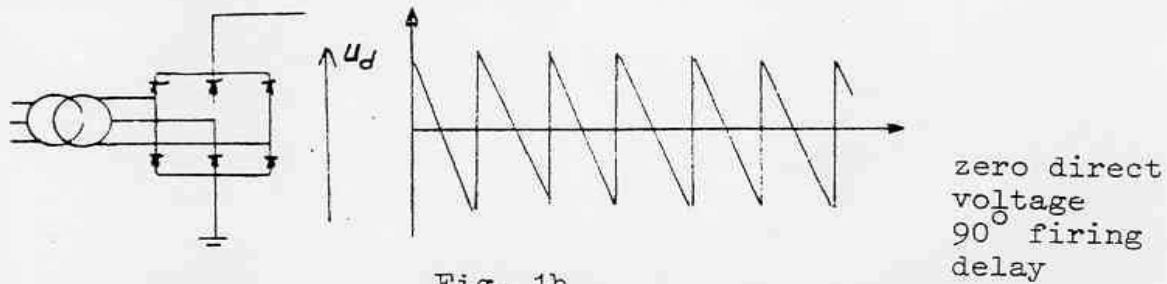


Fig. 1b

Convertor acts as synchronous condenser

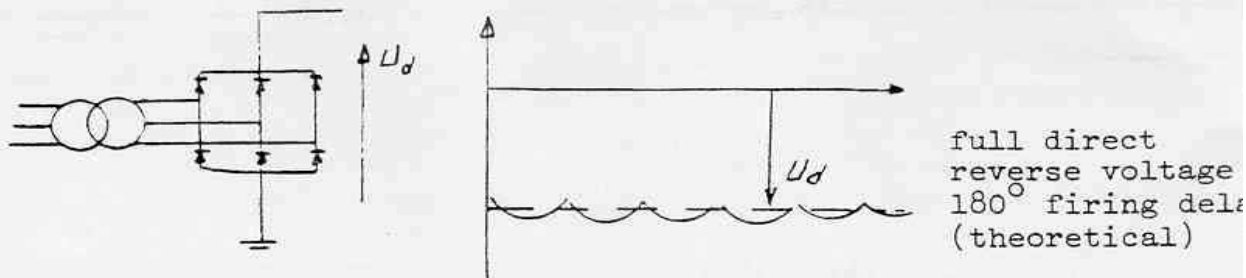
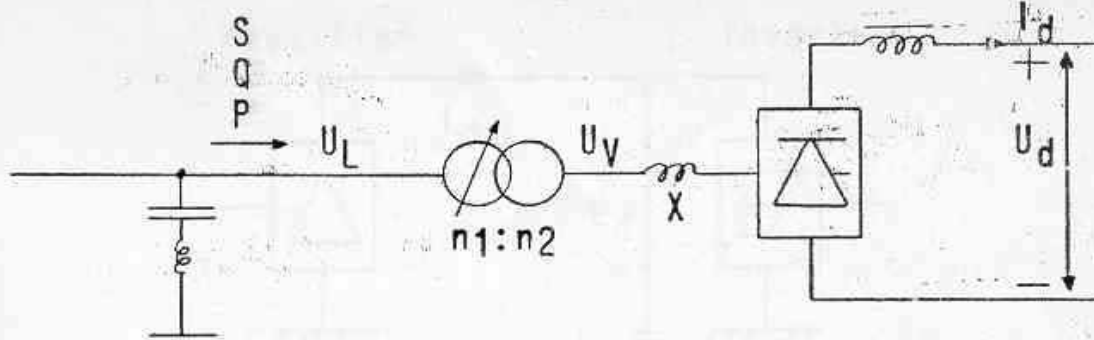


Fig. 1c



$$U_{dio} = \frac{3\sqrt{2}}{\pi} U_V = 1.35 U_V$$

$$U_V = \frac{n_2}{n_1} \cdot U_L$$

$$d_x = \frac{3}{\pi} \cdot \frac{X \cdot I_{dN}}{U_{dioN}}$$

Rectifier:
$$U_d = U_{dio} \left(\cos \alpha - d_x \cdot \frac{I_d}{I_{dN}} \cdot \frac{U_{dioN}}{U_{dio}} \right)$$

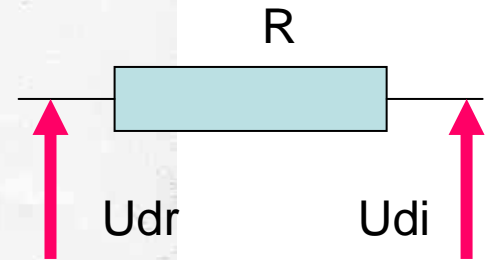
Inverter:
$$U_d = -U_{dio} \left(\cos \gamma - d_x \cdot \frac{I_d}{I_{dN}} \cdot \frac{U_{dioN}}{U_{dio}} \right)$$

$$P = I_d \cdot U_d$$

$$S = I_d \cdot U_{dio}$$

$$Q = +\sqrt{S^2 - P^2}$$

$$\cos \varphi = \frac{U_d}{U_{dio}}$$



$$U_{dr} - U_{di} = R I_d$$

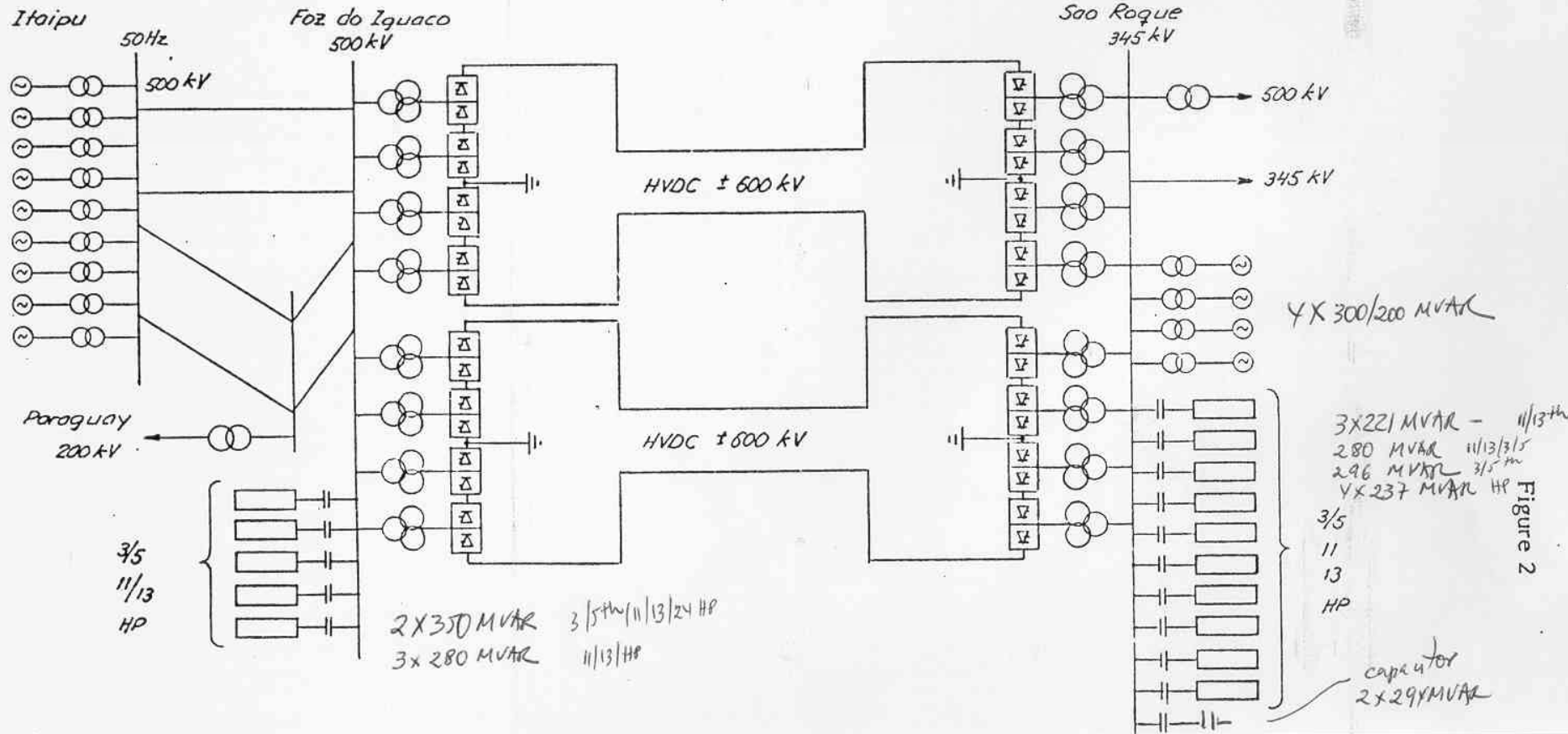
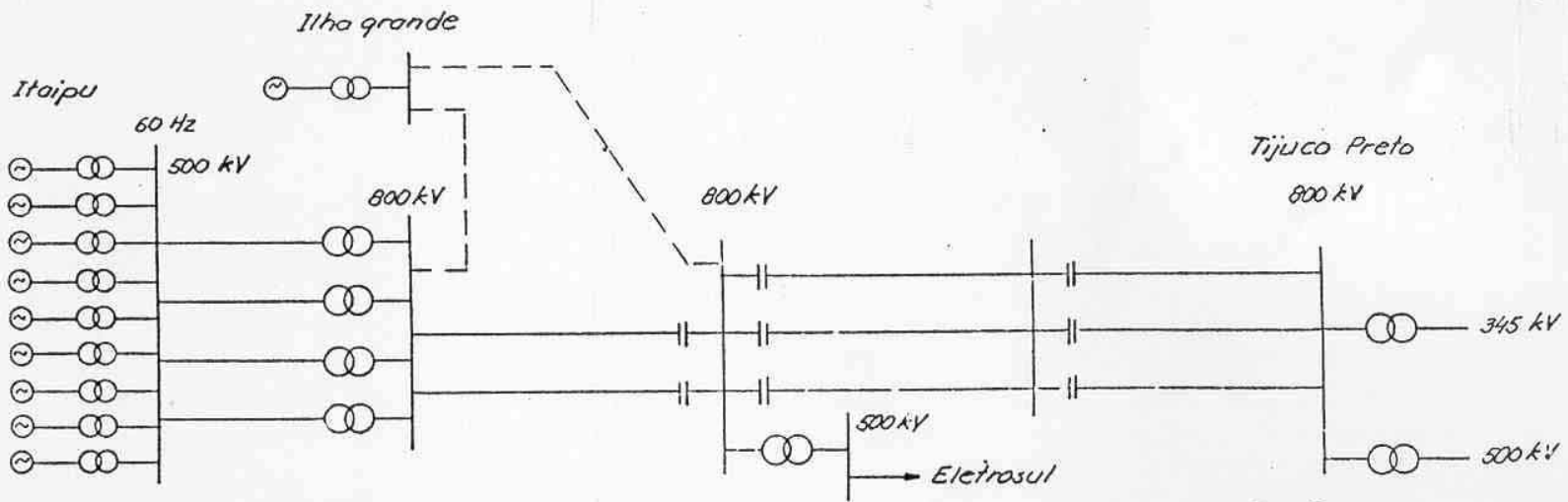


Figure 2

Sistemas CC existentes

- Válvula de mercúrio
- Tiristor

NELSON RIVER 1
1972 1976
310 MW 1620 MW
±300 KV ±450 KV
+150 KV

ENGLISH CHANNEL
1961
160 MW ±100 KV

KINGSNORTH
1975
640 MW ±266 KV

KONTI-SKAN
1965
250 MW 250 KV

GOTLAND
1954
20 MW 100 KV

VOLGOGRAD-DONBASS
1965
750 MW ±400 KV

SAKUMA 50-60 HZ
1965
300 MW 2x125 KV

VANCOUVER POL 1
1968 1969
78 MW 312 MW
130 KV 260 KV

PACIFIC INTERTIE
1970
1440 MW ±400 KV

SARDINIA
1967
200 MW 200 KV

NEW ZEELAND
1965
600 MW ±250 KV

VALDELA
MERCURIO



NELSON RIVER 2
 1978 1981 1982
 900 MW 1350 MW 1800 MW
 +250 KV +500 KV

SKAGERRAK
 1976 1977
 250 MW 500 MW
 +250 KV +250 KV

GOTLAND EXTENSION
 1970
 10 MW

FINLAND-RUSSIA
 1980
 1000 MW

TRI-STATE STEGALL
 1976
 100 MW

VANCOUVER POLE 2
 1976
 370 MW 280 KV

CU-PROJECT
 1978
 1000 MW +400 KV

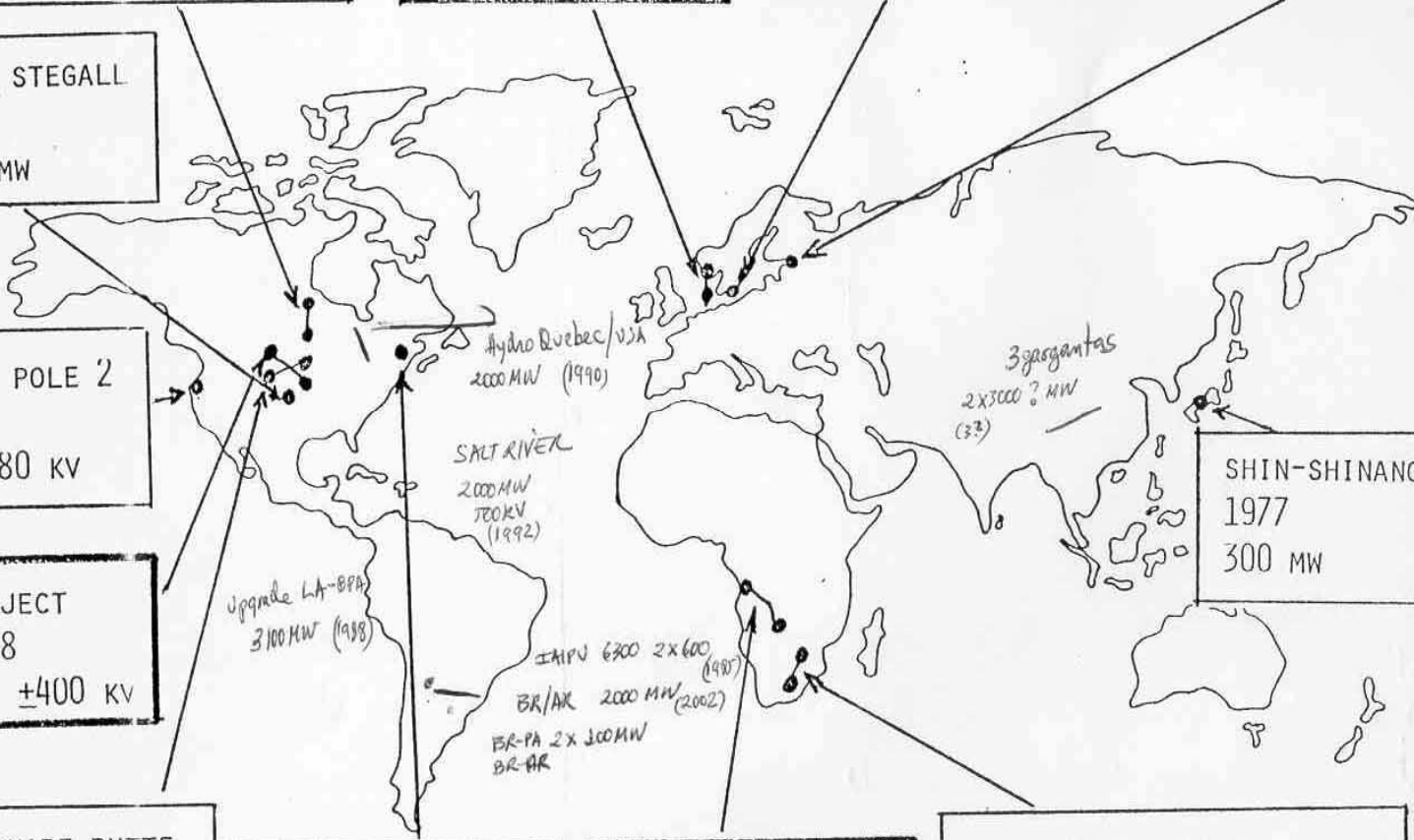
SQUARE BUTTE
 1977
 500 MW +250 KV

EEL RIVER
 1972
 320 MW 2x80 KV

1120 MW (1983)
 INGA-SHABA
 1978
 560 MW +500 KV

CABORA BASSA
 1975 1977 1979
 970 MW 1455 MW 1940 MW
 +266 KV +400 KV +533 KV

SHIN-SHINANO 50-60 HZ
 1977
 300 MW 600 MW

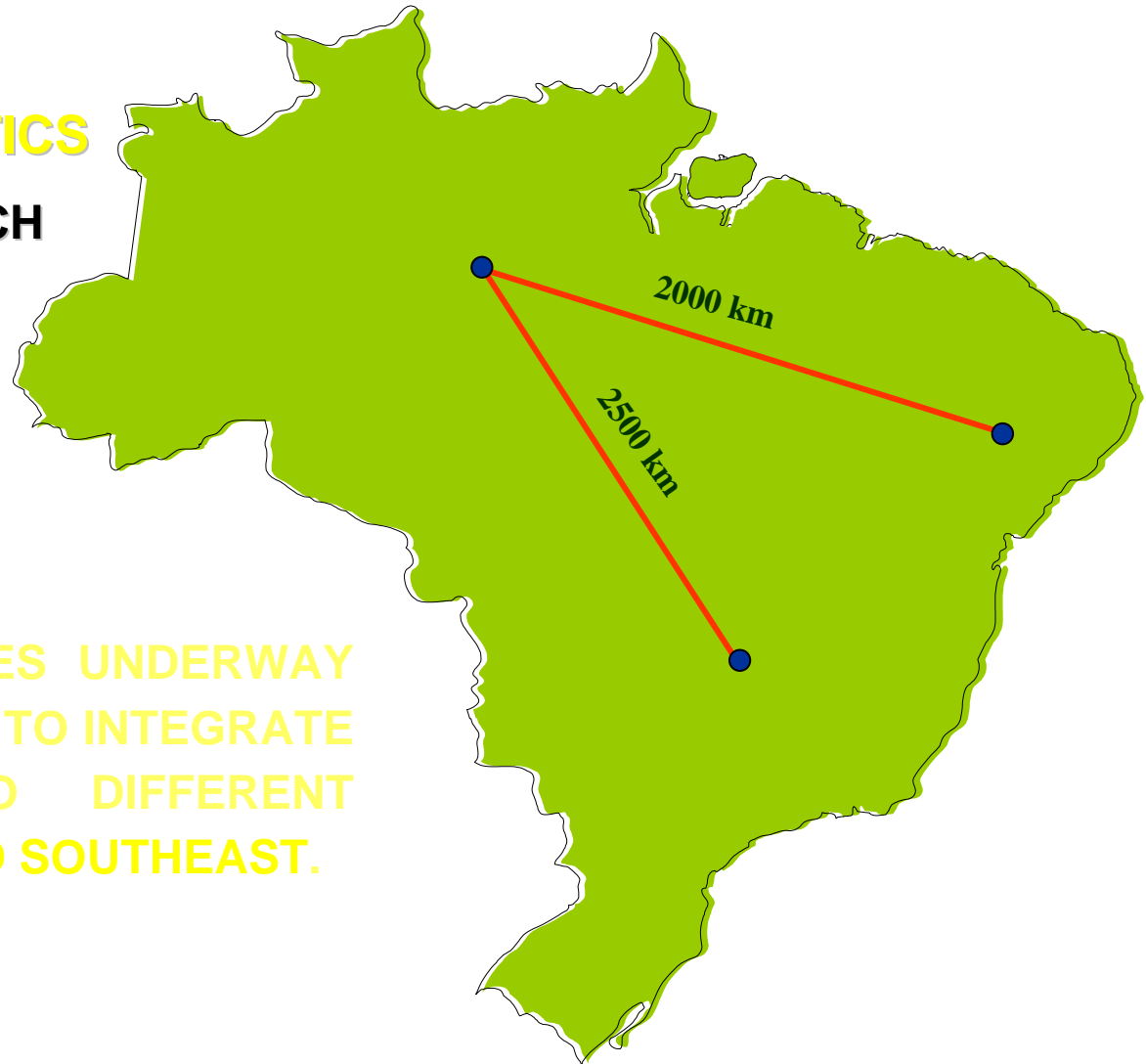


THYRISTOR

BELO MONTE POWER PLANT CONNECTION

PROJECT CHARACTERISTICS

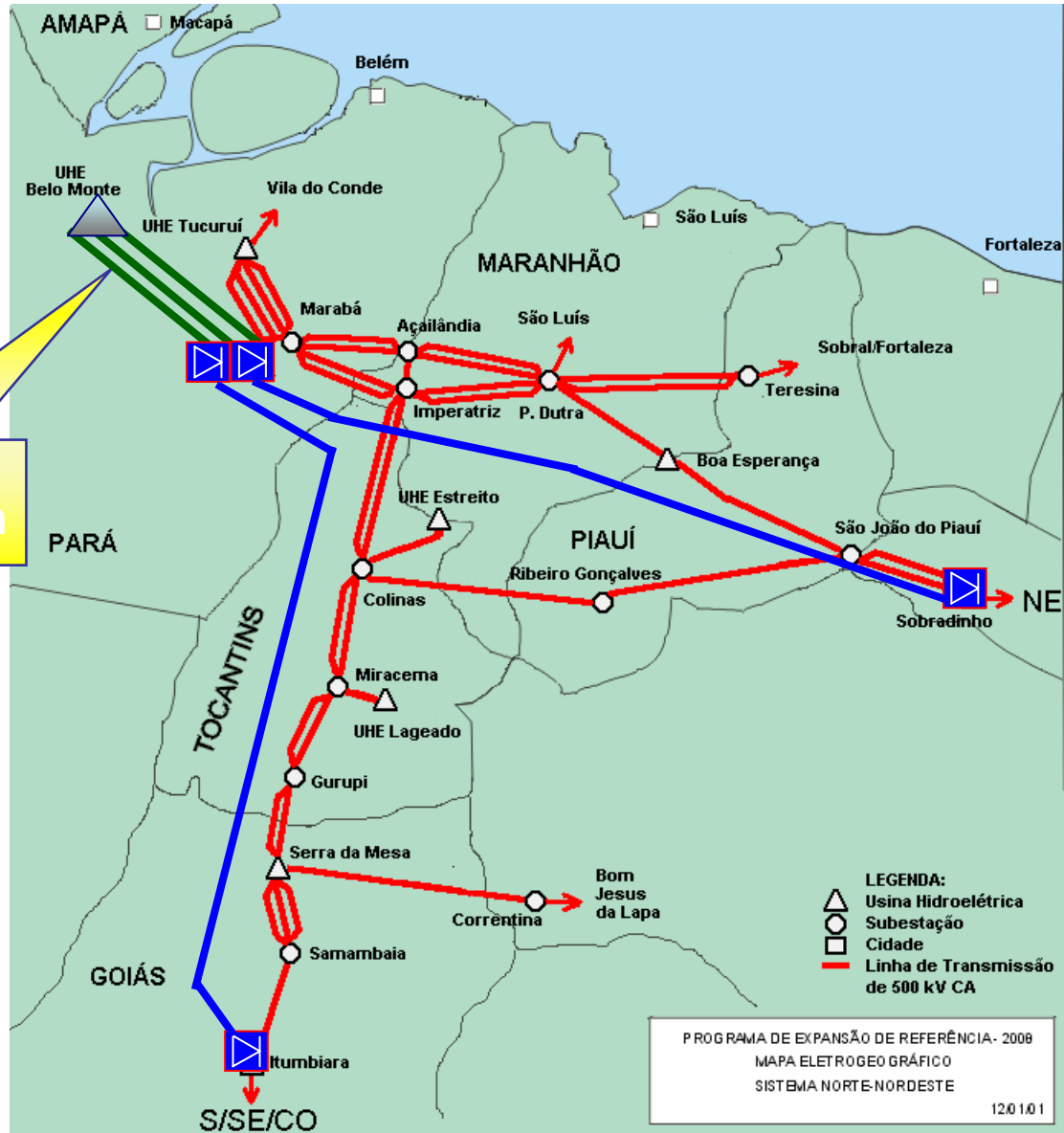
2 STAGES OF 5500 MW EACH



THE TRANSMISSION STUDIES UNDERWAY CONSIDER THE POSSIBILITY TO INTEGRATE BELO MONTE TO TWO DIFFERENT REGIONS: NORTHEAST AND SOUTHEAST.

CONNECTION

765 kV System



MADEIRA POWER PLANTS

PROJECT CHARACTERISTICS

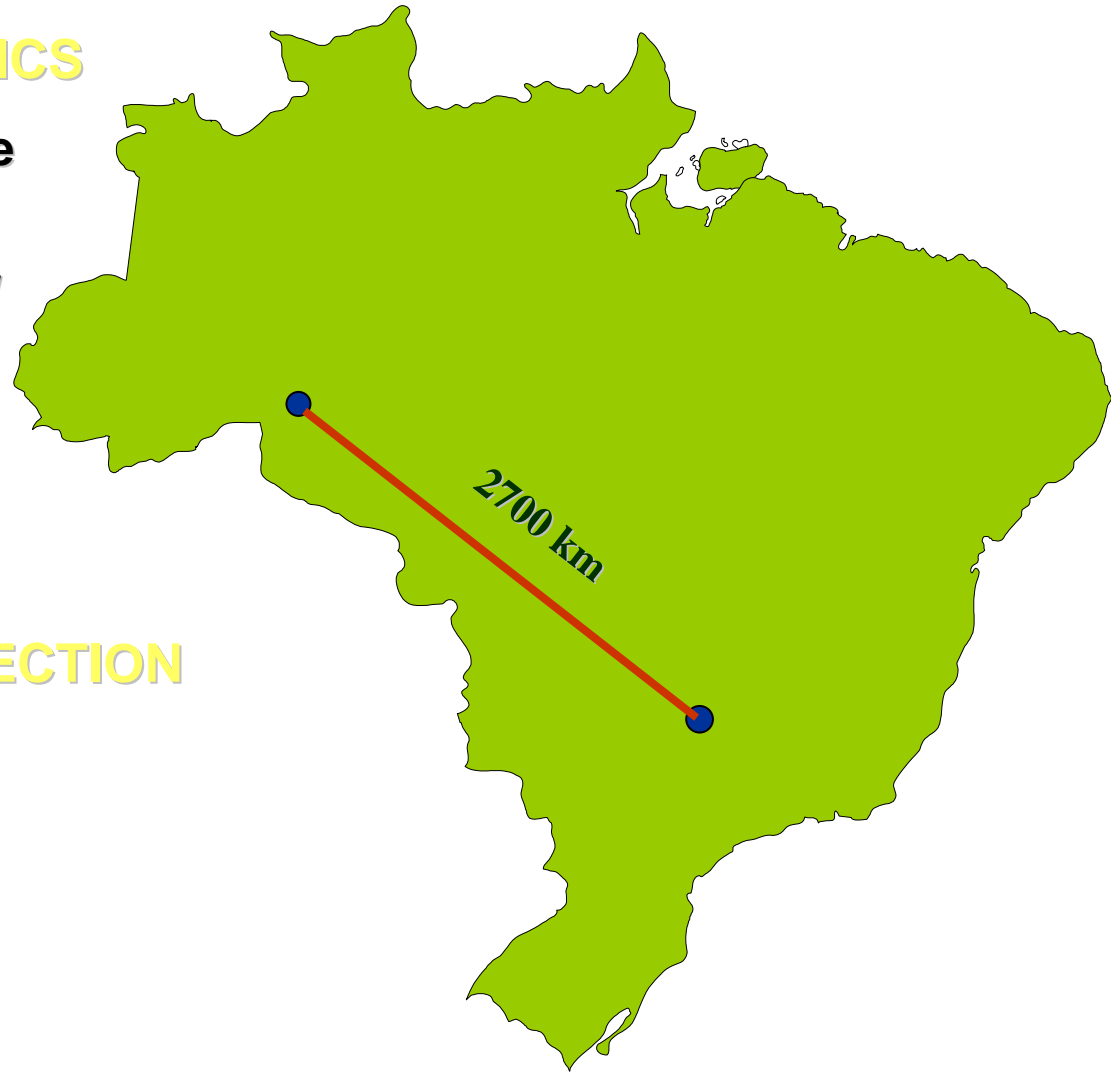
**2 POWER PLANTS: JIRAU e
S.ANTONIO**

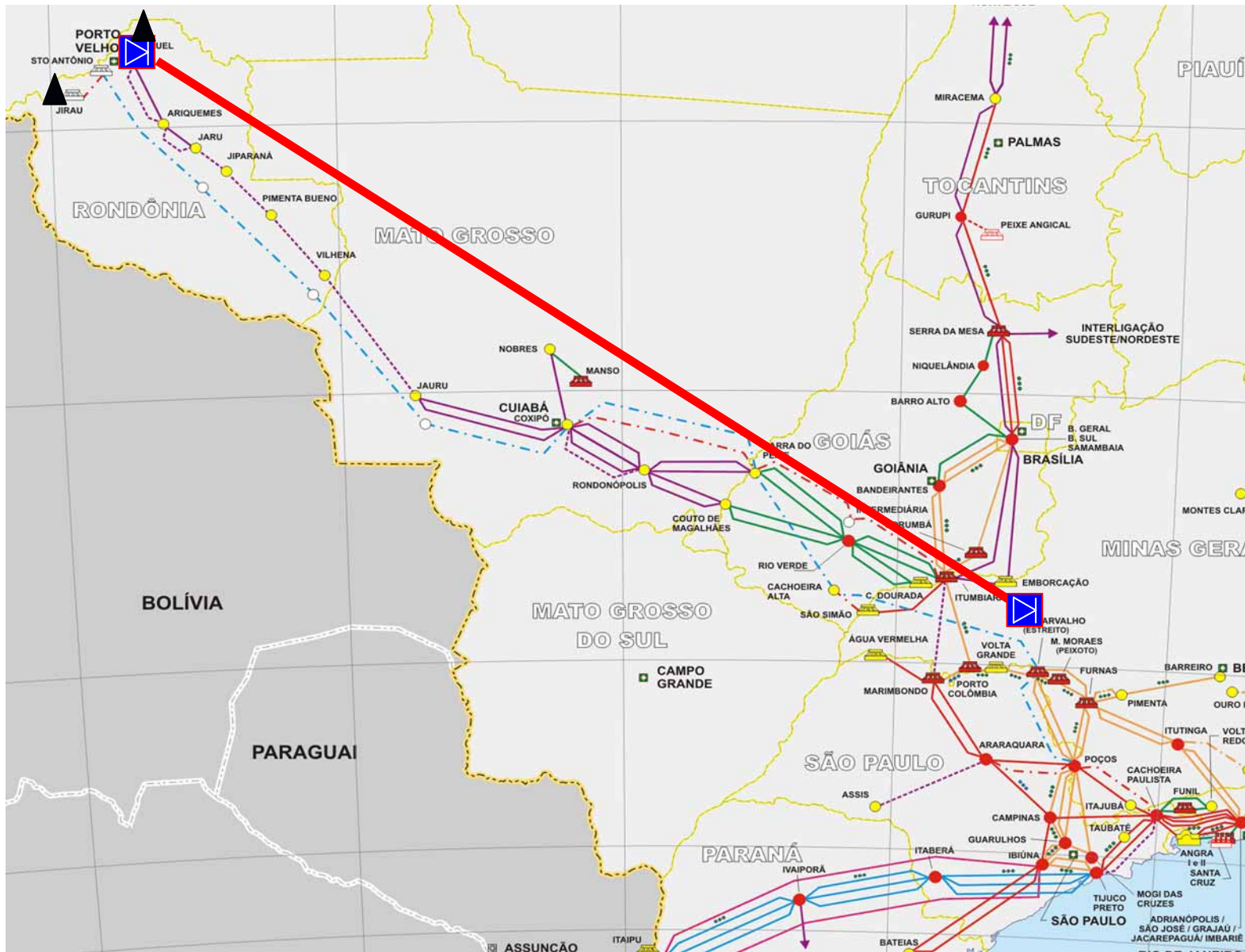
TOTAL POWER = 6300 MW

ALTERNATIVES FOR CONNECTION

AC – 500 and 765 kV

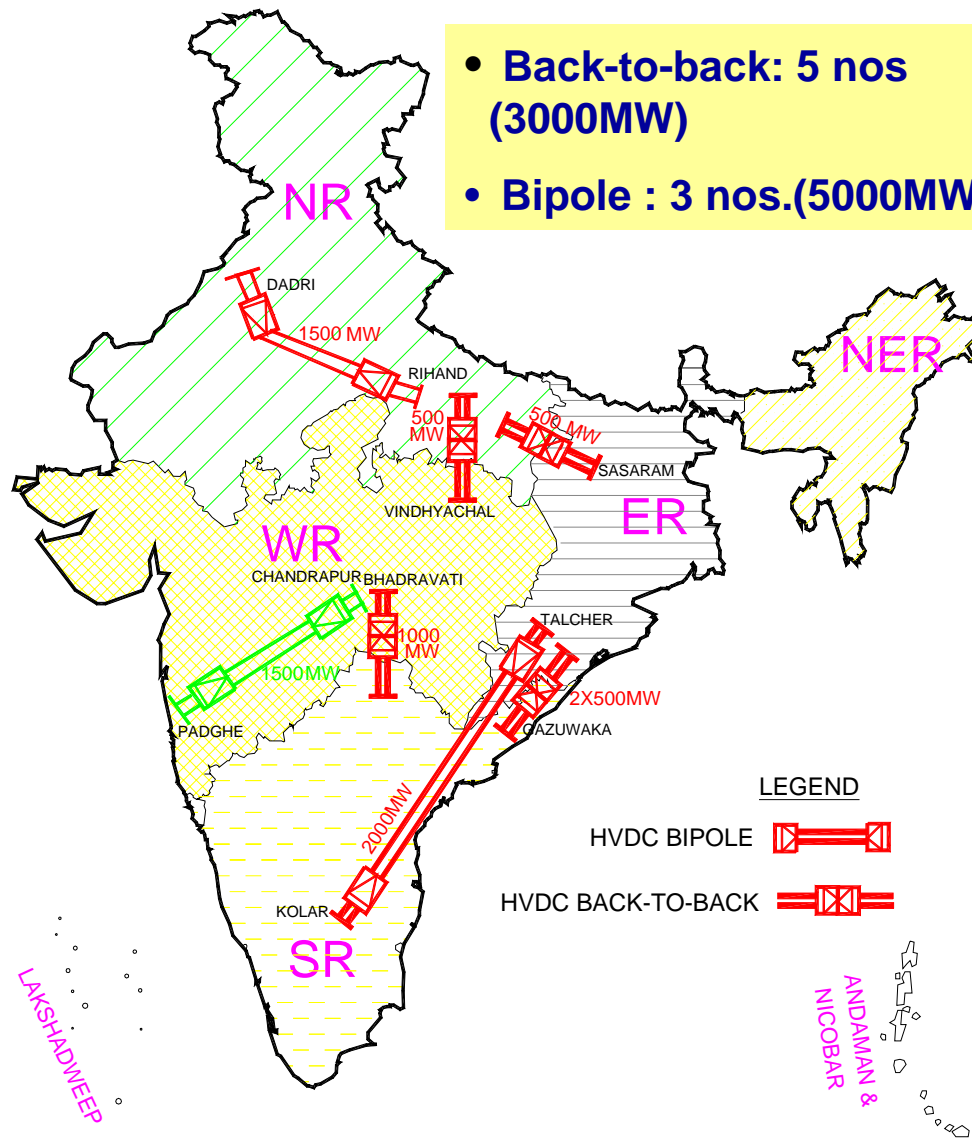
DC – ± 600 kV





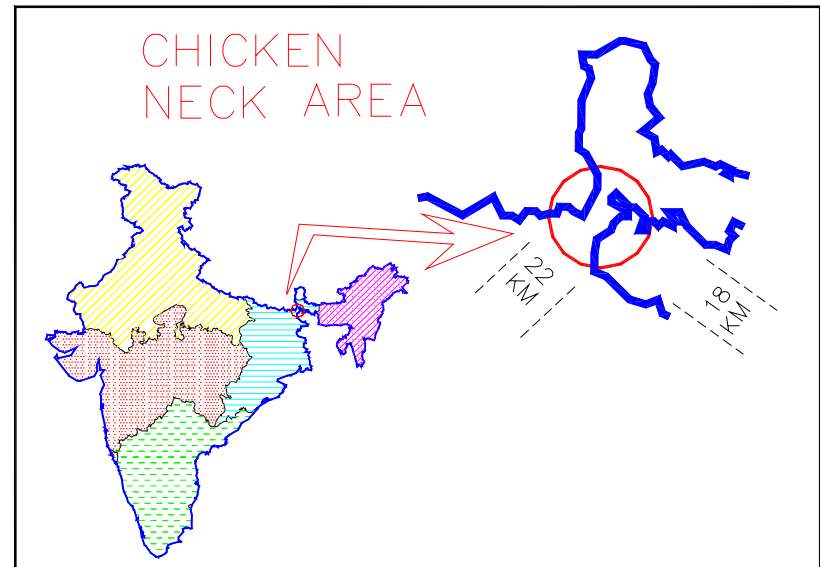
HVDC SYSTEMS- AT PRESENT

- Back-to-back: 5 nos (3000MW)
- Bipole : 3 nos.(5000MW)

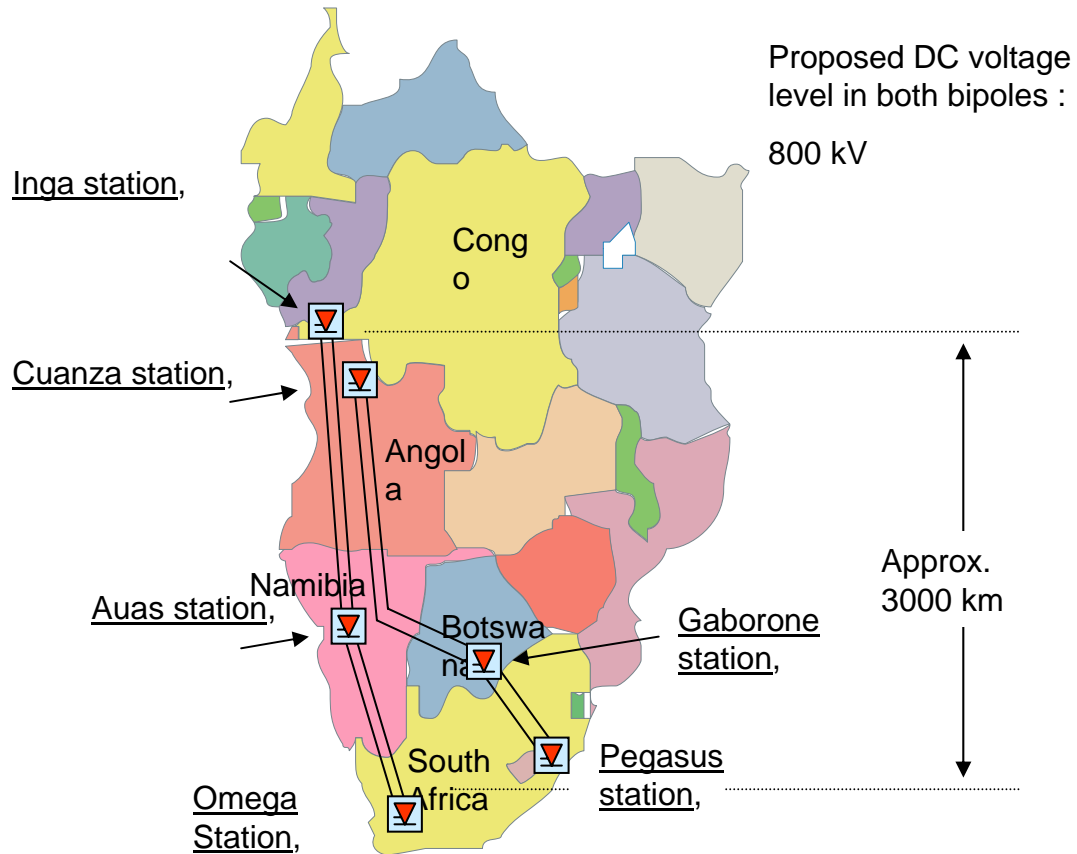
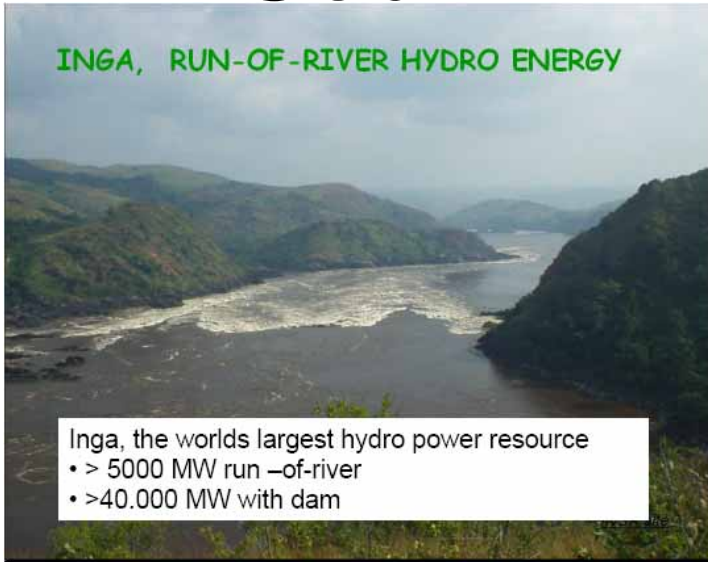


Consideration for Development of Transmission System

- 50000 MW power to be evacuated through Chicken Neck Area in North of West Bengal :
 - A very narrow (22 km. Wide) patch of land, 18 km near Siliguri having borders of Nepal on one side & Bangladesh on other and largely habited.
 - All transmission lines, Railway lines, gas pipe-lines, Telecommunication lines etc. have to pass through the Chicken neck area



South Africa: West Cor Line



Jinsha River I (Xiluodu, Xiangjiaba), Jingping & Xiaowan Dams, for 800kV UHVDC

Updated 2006-4-14, CNABB-PTSG

Xiangjiaba – Shanghai

800kV, 6400 MW, 1950km
2011

Xiluodu – Zhejiang

800kV, 6400 MW, 1870km
2015

Xiluodu – Hubei (C.China)

800kV, 6400 MW, 1070km
2014

Jingping – East China

800kV, 6400 MW, 2100km
2012

Yunnan – Guangdong

800kV, 5000 MW, 1500km
2009

